

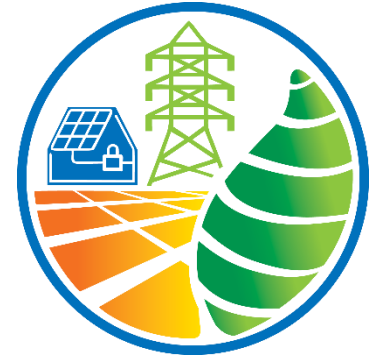


Droop-Control-Aided State Estimation in Active Distribution Systems

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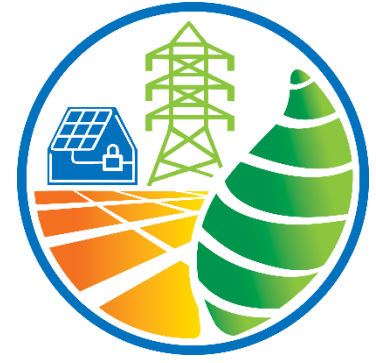


Introduction – 1

Background

- DRESs → **Increased** operational complexity of distribution grids
- Growing necessity for continuous **monitoring**
- **State estimation** as the main facilitator

- Main **attributes** of state estimation techniques:
 - Measurement noise removal
 - Bad data detection
 - Deliberately injected false data (**cybersecurity** breach)



Introduction – 2

State-of-the-art

- Main DSSE categories: **Model-free & Model-based**

Machine learning

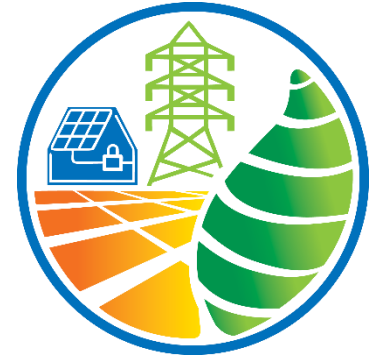
Robust optimization

Our Focus

- Several **variants** of model-based solutions exist aiming to improve
 - calculation performance
 - solution accuracy
- Common **drawback** → Local control logic of DRESs is **neglected**

Scope

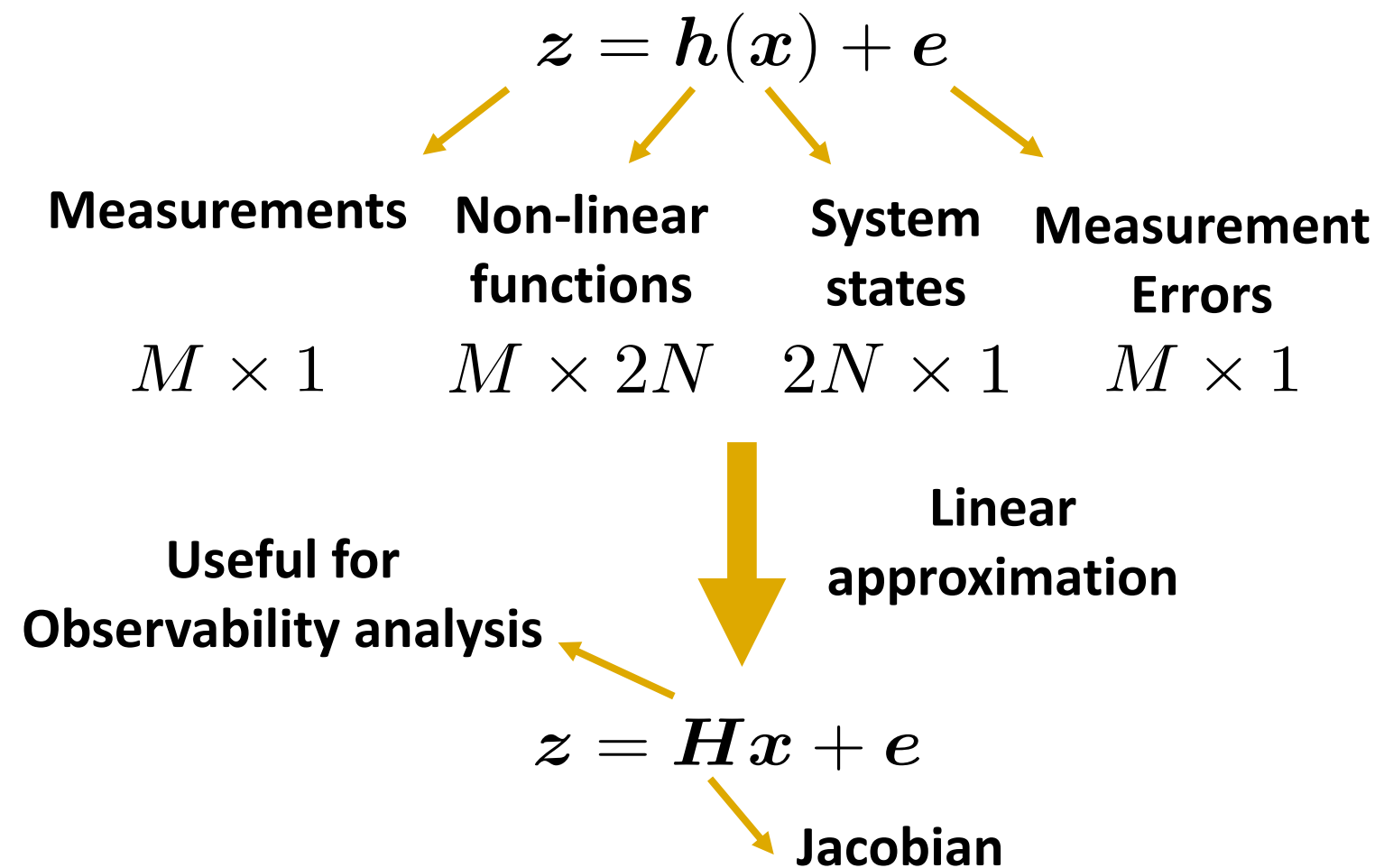
- **Enhance** DSSE performance by including local control logic (droop control)

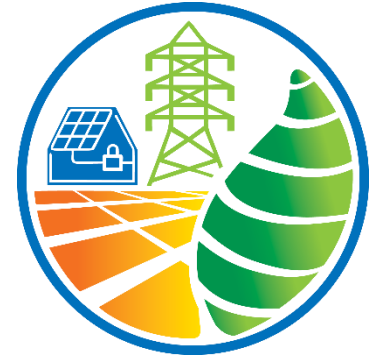


State Estimation Preliminaries

Problem Formulation

- Assuming an N bus system (excl. slack bus)





Conventional DSSE

- DSSE is formulated as an **optimization problem**

Objective function

$$\min \sum_{i \in \mathcal{M}_P} \frac{(P_i - \hat{P}_i)^2}{\sigma_{P_i}^2} + \sum_{i \in \mathcal{M}_Q} \frac{(Q_i - \hat{Q}_i)^2}{\sigma_{Q_i}^2} + \sum_{i \in \mathcal{M}_V} \frac{(V_i - \hat{V}_i)^2}{\sigma_{V_i}^2}$$

Estimated Measured
Measurement accuracy

Equality constraints

$$V_i = f(\mathbf{P}, \mathbf{Q}, V_{\text{prev},i}), i \in \mathcal{N}$$

Recursive non-linear power flow equations [1]

$$P_i = Q_i = 0, i \in \mathcal{N}_{\text{zero}}$$

Zero Injection buses

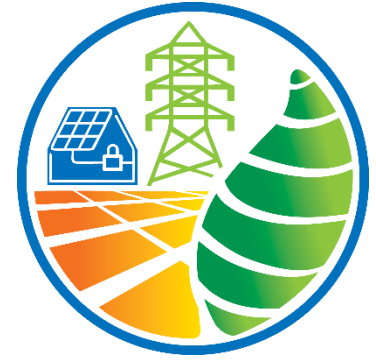
$$P_0 = \sum_{i \in \mathcal{N}, i \neq 0} P_i + P_{\text{loss,tot}}$$

Slack bus active power

$$Q_0 = \sum_{i \in \mathcal{N}, i \neq 0} Q_i + Q_{\text{loss,tot}}$$

Slack bus reactive power

[1] G. C. Kryonidis, C. S. Demoulias and G. K. Papagiannis, "A Nearly Decentralized Voltage Regulation Algorithm for Loss Minimization in Radial MV Networks With High DG Penetration," in *IEEE Transactions on Sustainable Energy*, vol. 7, no. 4, pp. 1430-1439, Oct. 2016, doi: 10.1109/TSTE.2016.2556009.



Proposed Method

Objective function

$$\min \sum_{i \in \mathcal{M}_P} \frac{(P_i - \hat{P}_i)^2}{\sigma_{P_i}^2} + \sum_{i \in \mathcal{M}_Q} \frac{(Q_i - \hat{Q}_i)^2}{\sigma_{Q_i}^2} + \sum_{i \in \mathcal{M}_V} \frac{(V_i - \hat{V}_i)^2}{\sigma_{V_i}^2}$$

Equality constraints

$$V_i = f(\mathbf{P}, \mathbf{Q}, V_{\text{prev},i}), i \in \mathcal{N}$$

Recursive non-linear power flow equations

$$P_i = Q_i = 0, i \in \mathcal{N}_{\text{zero}}$$

Zero Injection buses

$$P_0 = \sum_{i \in \mathcal{N}, i \neq 0} P_i + P_{\text{loss,tot}}$$

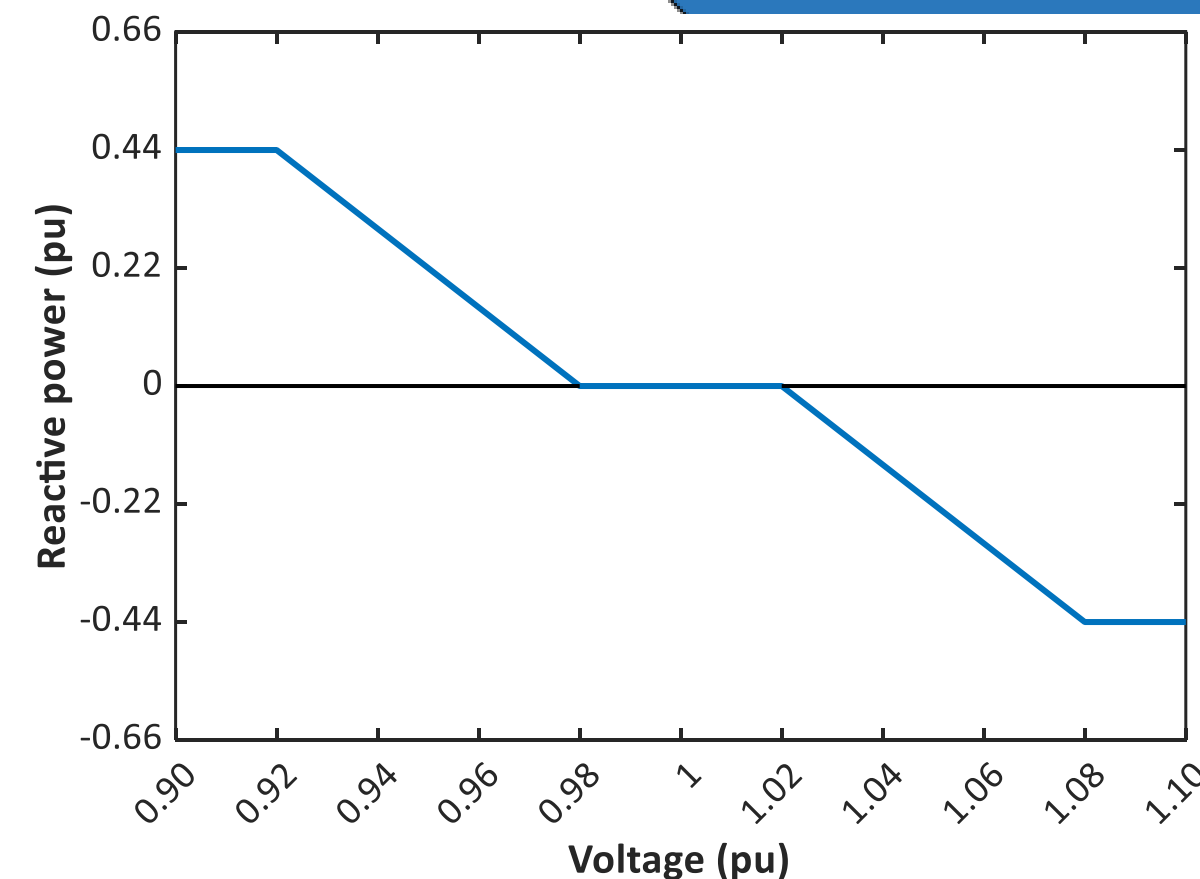
Slack bus active power

$$Q_0 = \sum_{i \in \mathcal{N}, i \neq 0} Q_i + Q_{\text{loss,tot}}$$

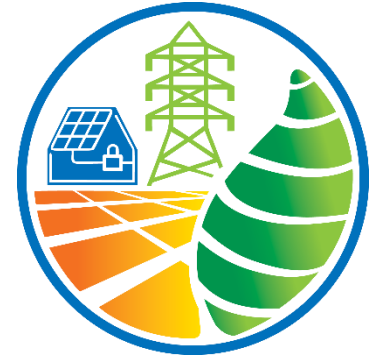
Slack bus reactive power

$$Q_i = g(V_i), i \in \mathcal{N}_{DRES}$$

Q(V) droop control [2] →



[2] IEEE Std 1547-2018, "IEEE Standard for Interconnection and Interoperability of Distributed Energy Resources with Associated Electric Power Systems Interfaces," IEEE Std 1547-2018 (Revision of IEEE Std 1547-2003), pp. 1–138, 2018.



System Under Study

- A radial, 20 kV DS in Greece (16 PVs)

- **Operating scenario**

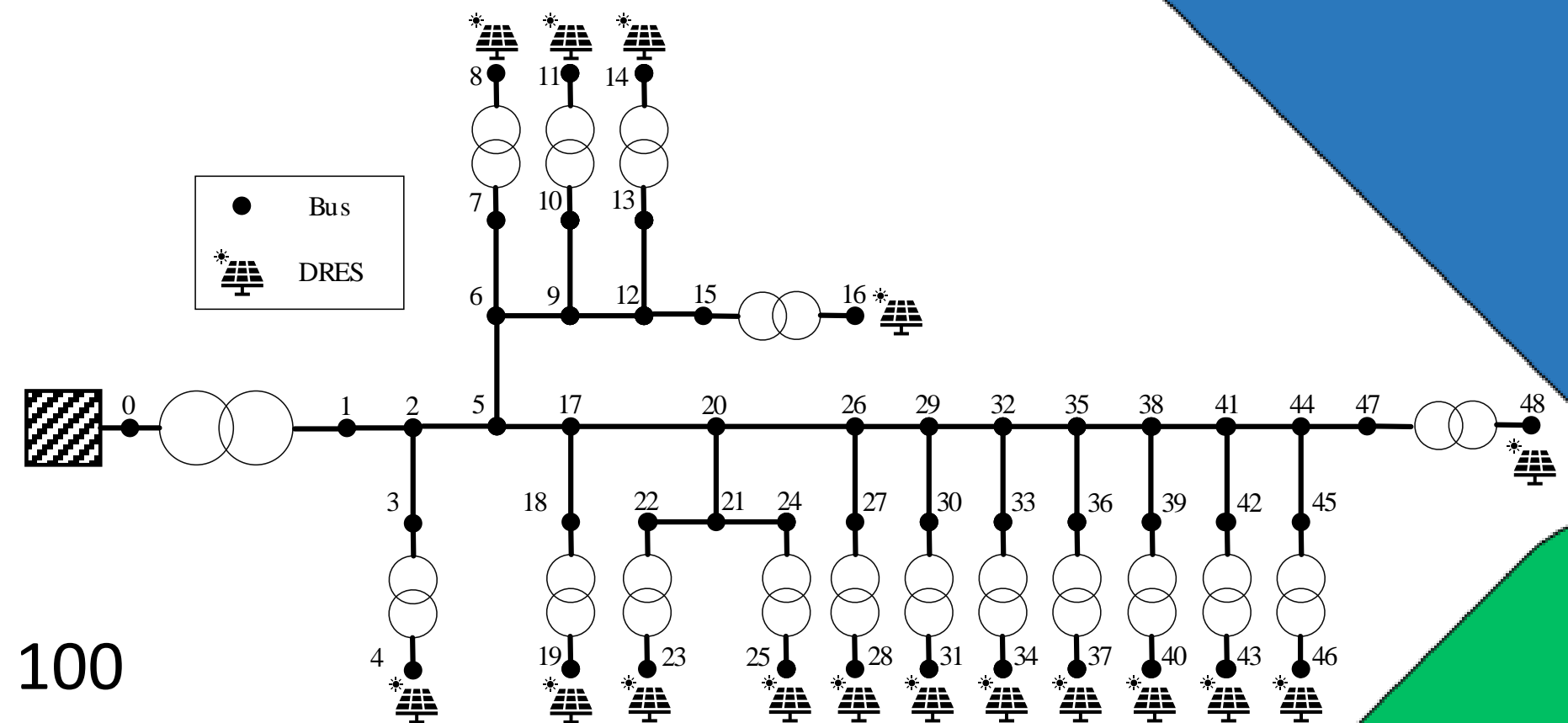
$$Q_{max,i} = 0.44 \cdot S_{r,i}, i \in \mathcal{N}_{DRES}$$

$$P_i^{oper} = \sqrt{S_{r,i}^2 - Q_{max,i}^2}, i \in \mathcal{N}_{DRES}$$

- **Measurements accuracy**

$$\sigma_{P_i} = 0.012 \quad \sigma_{Q_i} = 0.015 \quad \sigma_{V_i} = 0.01$$

- Different measurement errors using 100 Monte Carlo simulations





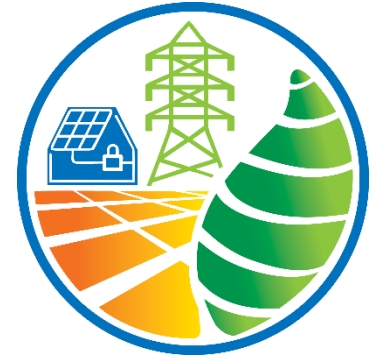
Impact on Accuracy – Single MC case

Absolute percentage error (APE) as the main evaluation Index

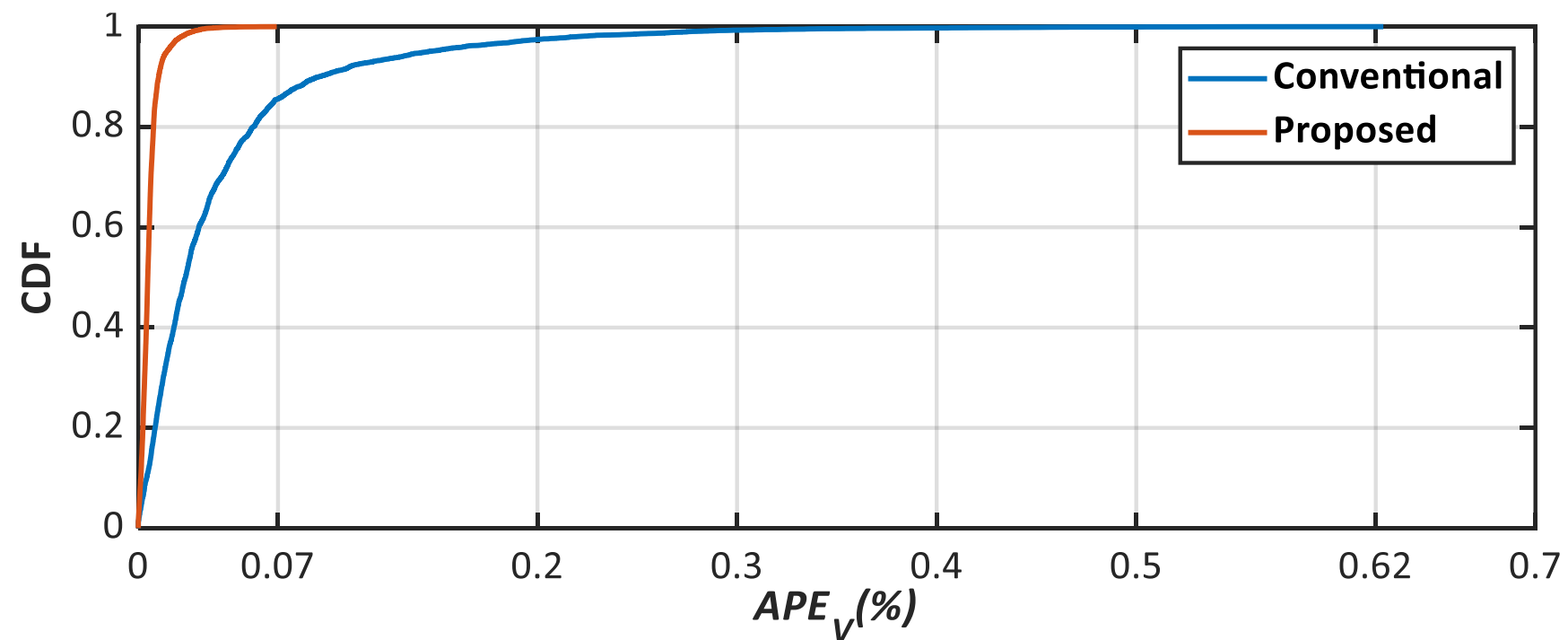
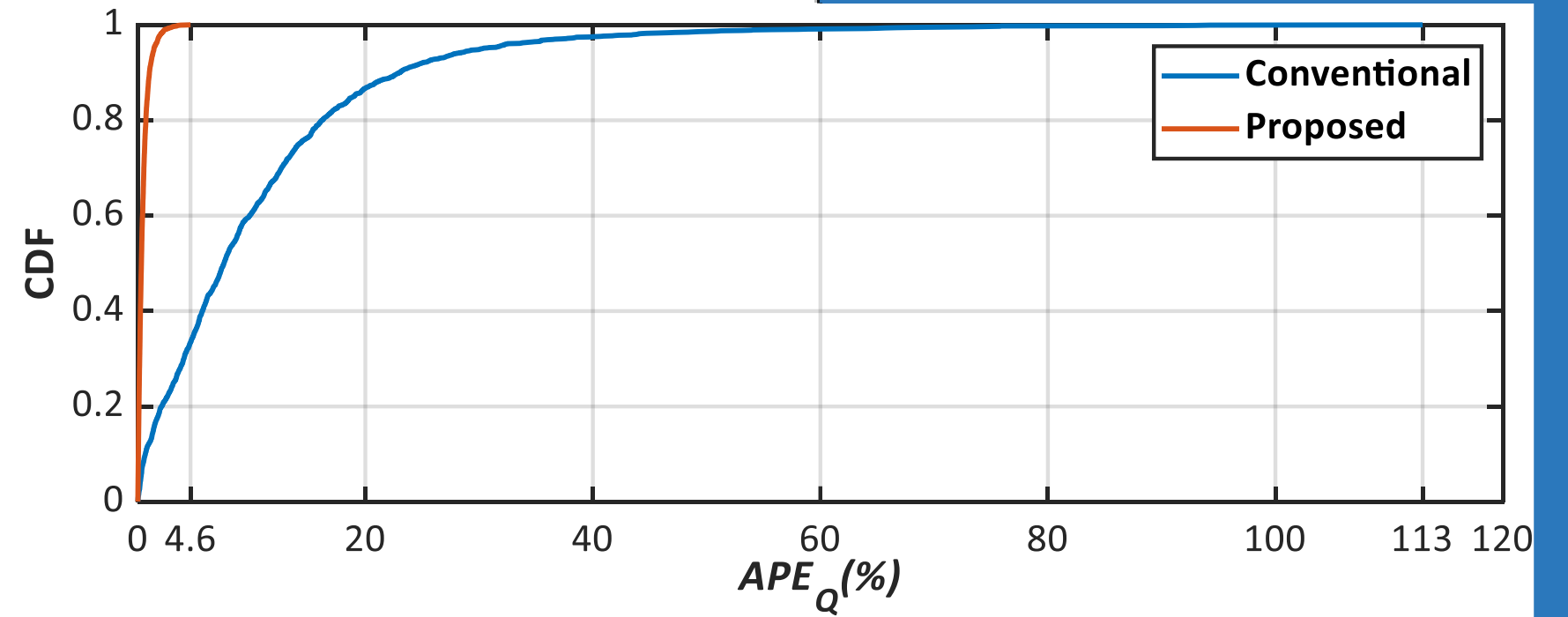
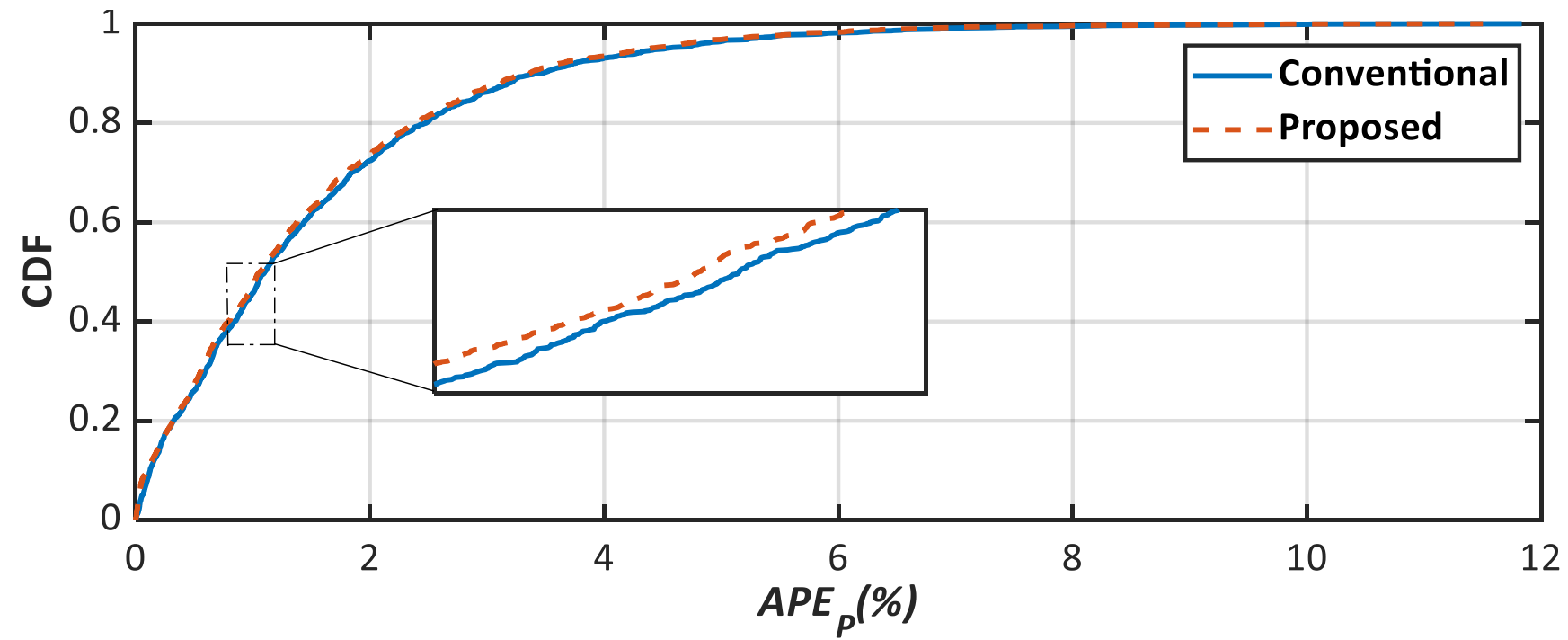
$$\underbrace{APE_{X_i}(\%)}_{P_i, Q_i, V_i} = \frac{\overset{\text{Estimated}}{X_i} - \overset{\text{True value}}{X_i^{true}}}{X_i^{true}} \cdot 100\%$$

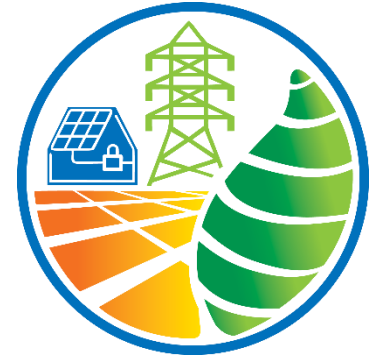
Table 1: Comparison of $APE_{X_i}(\%)$

i	Conventional method			Proposed method		
	P_i	Q_i	V_i	P_i	Q_i	V_i
4	0.42	8.69	0.015	0.4	1.04	0.0028
11	0.46	3.06	0.021	0.45	0.28	0.0032
16	0.52	4.24	0.042	0.5	0.08	0.0077
23	0.75	5.76	0.057	0.73	0.01	0.0092
28	0.25	1.28	0.004	0.24	0.21	0.0038
37	1.13	8.99	0.062	1.1	0.45	0.0011
43	4.9	24.83	0.297	4.76	0.99	0.0333
48	0.67	3.79	0.029	0.65	0.19	0.0042



Impact on Accuracy – All MC cases





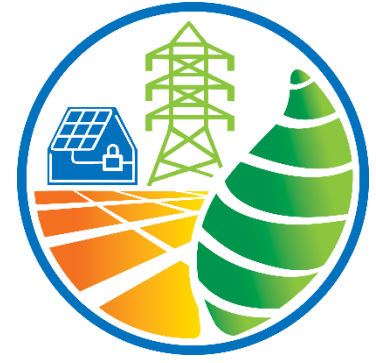
Impact on Accuracy – Main Observations

Conventional method

- Worst estimates for **reactive power** in conventional method
- This is mainly attributed to the **decreased** measurement accuracy

Proposed method

- The proposed method leads to **considerably lower** APE_{Q_i} and APE_{V_i}
- The estimation accuracy of active power estimates is **slightly increased**



Impact on Observability

Observability criterion : Full-column rank of matrix H

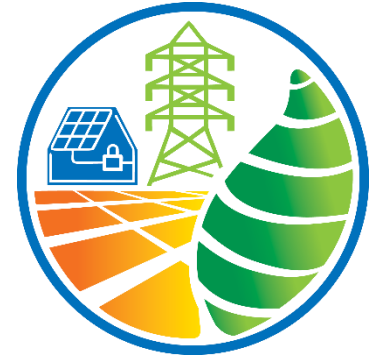
Conventional method: H

Proposed method: $H_{aug} = [H^T H_{droop}^T]^T$

Table 1: Minimum Observability Requirements

Method	Measurements Number	Meter Type
Conventional	30	Power meters
Proposed	15	Voltage sensors

50% less
measurements



Conclusions

- An **enhanced DSSE** technique is proposed integrating the local control logic of DRESs
- Simulations verified **higher estimation accuracies** for all monitored quantities and especially for **reactive power** and **voltage**
- DS observability **can be ensured** even under limited data resources
- The proposed method could **facilitate** the application of DSSE, allowing for the reliable monitoring of modern, active DSs

PARTNERS



Cuerva*



Thank you!



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